

Supporting Information

Robust and efficient membrane contactor for carbon dioxide capture enabled by thin-film composite Janus membrane

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1. Membrane fabrication procedures

The fabrication process for the TFC Janus membrane is schematically illustrated in Fig. S1a, while the fabrication of the monolithic PVDF membranes with varying hydrophobicities is depicted in Fig. S1b.

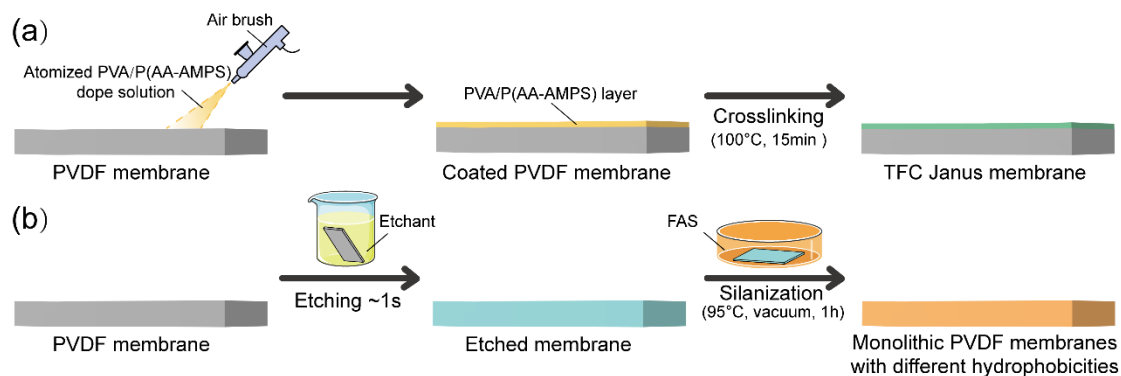


Fig. S1 Schematics illustrating the fabrication processes of (a) the TFC Janus membrane and (b) monolithic PVDF membranes with varying hydrophobicities.

2. Microstructure of the pristine PVDF membrane

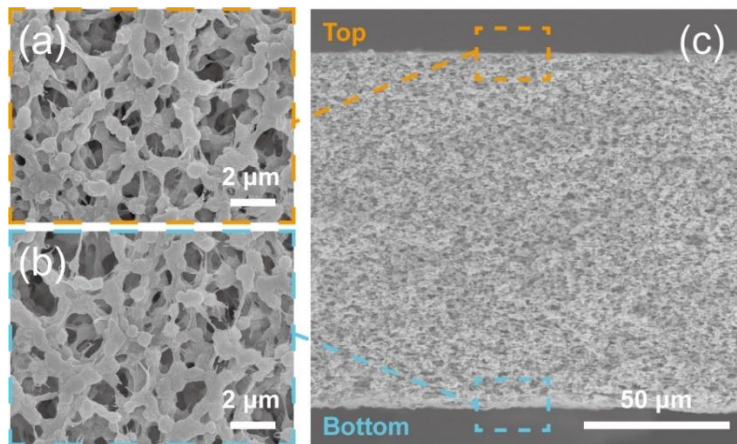


Fig. S2 SEM images of the pristine PVDF membrane: (a) top surface, (b) bottom surface, and (c) cross-section.

3. Solute filtration tests

The mean pore size and pore size distribution of the PVA surface layer on the TFC Janus membrane were determined using the experimental setup illustrated in Fig. S3.

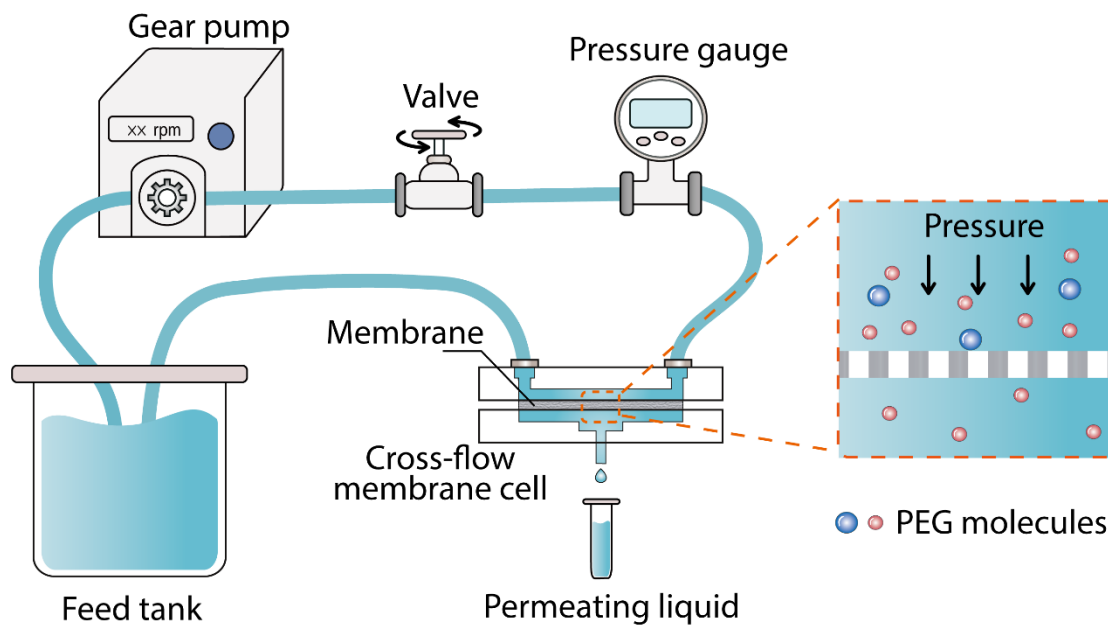


Fig. S3 Schematic diagram of the solute filtration test setup. The hydraulic pressure was controlled using a gear pump and a valve, with pressure measurements taken via a pressure gauge.

The solute filtration tests were performed with four feed solutions containing 200 ppm polyethylene glycol (PEG) with molecular weights of 400, 600, 1000, and 1500 Da. Before testing, the TFC Janus membrane was pre-wetted with ethanol and thoroughly rinsed with DI water. The membrane was then assembled into the testing cell, and the PEG solution was pumped towards the membrane under a hydraulic pressure of 6 bar.

The PEG concentration in the permeate (c_p) was measured using a total organic carbon analyzer (TOC-L, Shimadzu, Japan). Given the known feed PEG concentration ($c_f = 200$ ppm), the PEG rejection (R) was calculated as

$$R = \left(1 - \frac{c_p}{c_f}\right) \times 100\% \quad (\text{S1})$$

The Stokes diameter of PEG (d_s) was determined based on its molecular weight (M_w),

$$d_s = 33.46 \times 10^{-12} M_w^{0.557} (\leq 35,000) \quad (\text{S2})$$

The mean pore size (μ_s) of the PVA layer was defined as the d_s value corresponding to $R = 50\%$. The pore size distribution of the tested membrane was then calculated using the following relationship,

$$\frac{dR(d_p)}{d(d_p)} = \frac{1}{d_p \sqrt{2\pi} \ln \sigma_p} \exp \left[-\frac{(\ln d_p - \ln \sigma_p)^2}{2(\ln \sigma_p)^2} \right] \quad (\text{S3})$$

where d_p is the pore diameter, and σ_p is the geometric standard deviation, determined from the ratio of d_s values at $R = 84.13\%$ and $R = 50\%$.

4. Gas permeability measurements

We assessed the effect of the modification process on membrane structure by comparing the gas permeability of the membranes before and after modification. Gas permeability was measured using the setup illustrated in Fig. S4. A dried membrane sample with an effective area of 3 cm^2 was placed in a dead-end testing cell. A 15 vol% CO_2/N_2 gas mixture was directed into the testing cell at room temperature, with an applied pressure incrementally increased. The gas flow rate exiting the testing cell was recorded as a function of the applied pressure, allowing the gas permeability to be calculated. Each membrane underwent three independent measurements, and the averaged results with error bars were reported.

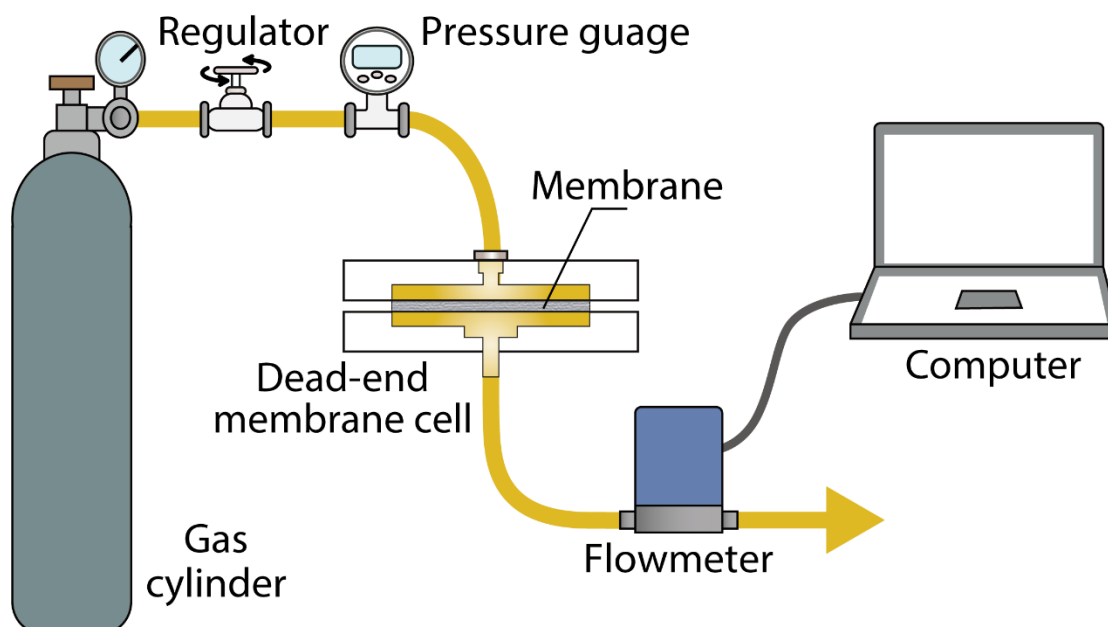


Fig. S4 Schematic diagram of the experimental setup for gas permeability measurements. The applied pressure on the gas stream was controlled using a regulator and monitored with a pressure gauge. The gas flow rate exiting the testing cell was measured with a flowmeter connected to a computer.

5. Diffusion experiments

We performed diffusion experiments to measure the MEA permeability of the monolithic PVDF membrane and the TFC Janus membrane. Prior to the experiments, a series of MEA solutions with concentrations of 0.001 mol/L, 0.01 mol/L, 0.1 mol/L, 0.5 mol/L, 1 mol/L, and 2 mol/L were prepared, and their corresponding pH values were measured using a pH meter (Thermo Scientific, Orion Star A214, USA) to establish the relationship between MEA concentration (C) and pH.

In each diffusion experiment, a small membrane coupon (1 cm^2) was pre-wetted with ethanol, rinsed with DI water, and mounted in a two-chamber diffusion cell (Fig. S5). The two chambers were filled with 5 mol/L MEA solution and DI water, respectively. The pH of the DI water chamber was continuously monitored over time, enabling the calculation of MEA concentration in that chamber. Using the time-dependent MEA concentration, the MEA permeability of the membrane was determined.

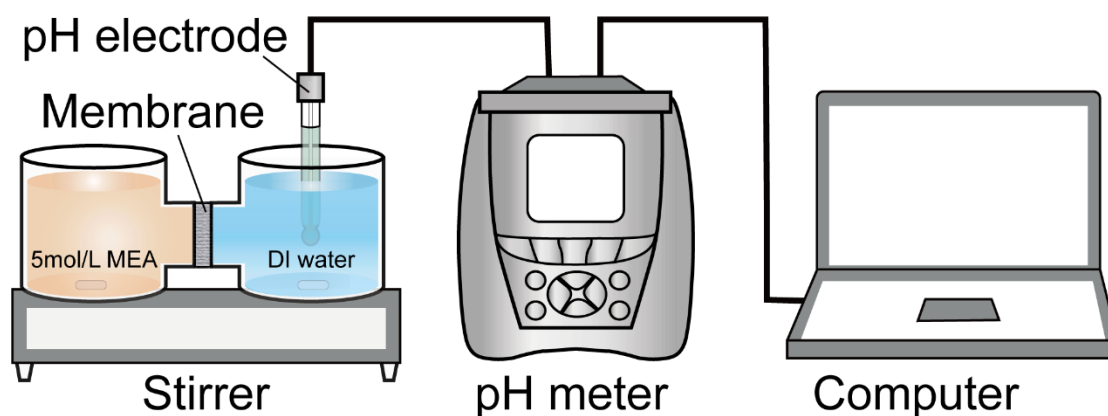


Fig. S5 Schematic diagram of the setup used in diffusion experiments.

6. Gas-Liquid membrane contactor (GLMC) experiments for CO₂ absorption

The setup for the GLMC experiments is shown in Fig. S6. At the start of each experiment, a mixed gas stream (i.e., 15 vol% CO₂/N₂) was introduced into one side of the membrane cell for 30 min to purge any air. Subsequently, the absorbent stream (1 mol/L MEA solution) was introduced into the other side of the membrane cell. The effective membrane area in the cell was 2 cm × 4 cm.

To minimize the impact of pulse flow on the results, a pulse damper was installed in the absorbent stream, and digital pressure gauges were used to monitor hydraulic pressures. The flow rate of the inlet mixed gas was maintained at 170 sccm using a gas mass flow controller (MFC, Sevenstar, D07-19, China), while the flow rate of the MEA solution was controlled at 0.3 L/min by a peristaltic pump. To prevent the formation of gas bubbles in the MEA solution, the pressure of the mixed gas was kept ~10 kPa lower than that of the MEA solution.

As the mixed gas passed through the GLMC cell, CO₂ was absorbed by the MEA solution. A gas flowmeter (GFM, Sevenstar, CS200, China) and a CO₂ analyzer (Wandi, PDA600, China) continuously monitored the flow rate of the mixed gas and the CO₂ concentration, respectively. Using the measured flow rate and CO₂ concentration data, the real-time CO₂ flux (J_{CO_2} , mol/m²/s) in the GLMC system could be calculated,

$$J_{CO_2} = \frac{P(C_{in}Q_{in} - C_{out}Q_{out})}{A_mRT} \quad (S4)$$

where C_{in} and C_{out} are the CO₂ concentrations (vol%) at the inlet and outlet of the membrane cell, respectively, Q_{in} and Q_{out} are the volume flow rates of the mixed gas (m³/s) at the inlet and outlet, respectively, P is the pressure of the gas mixture (atm), A_m is the effective area of the membrane (m²), R and T are the ideal gas constant and operating temperature, respectively.

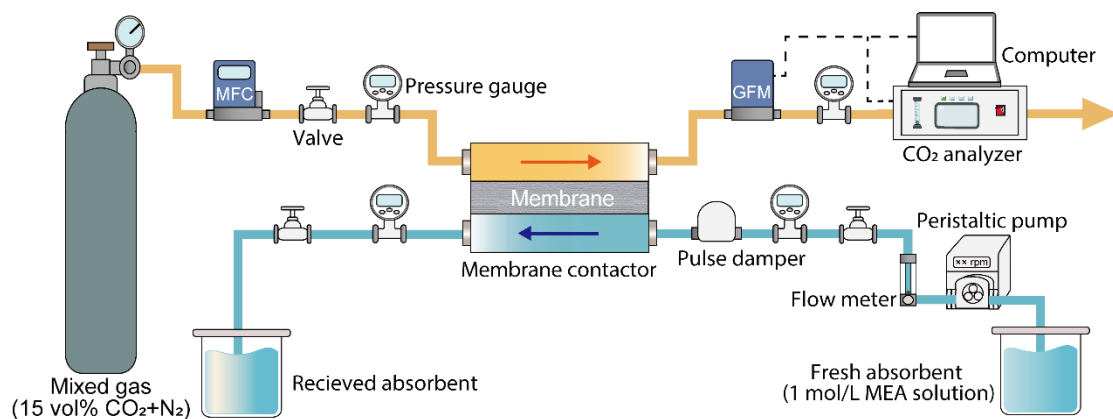


Fig. S6 Schematic diagram of the setup used for the GLMC experiment.

7. Electrochemical impedance tests

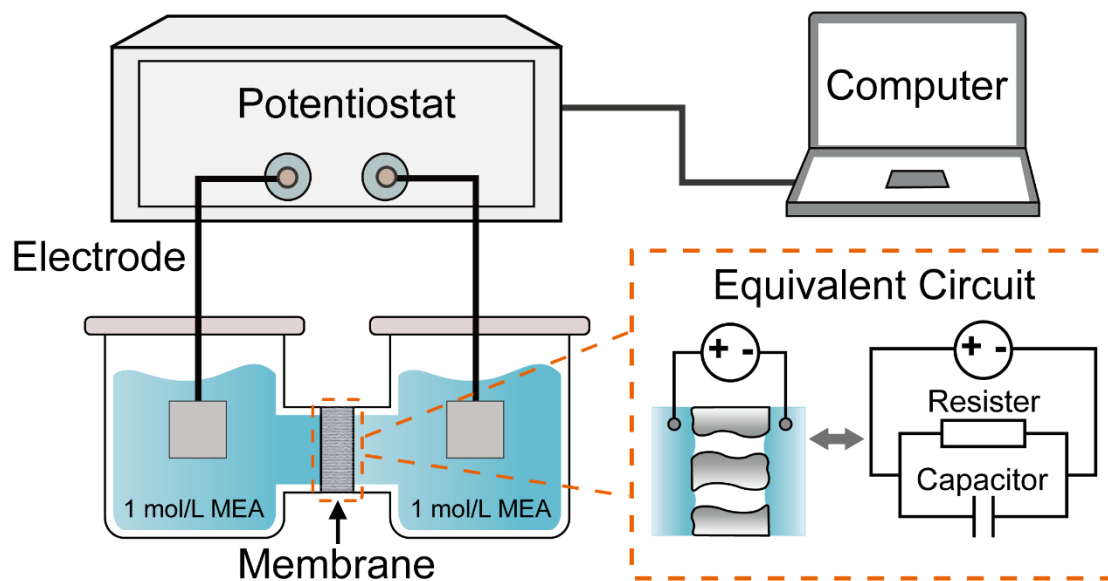


Fig. S7 Schematic diagram of the experimental setup for electrochemical impedance tests.

8. UTDR tests

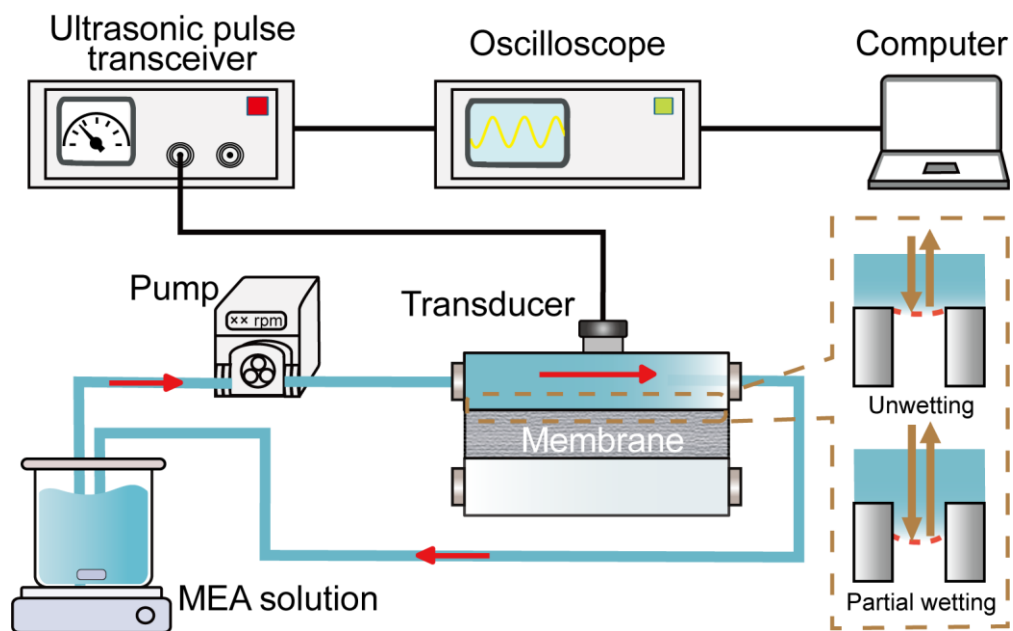


Fig. S8 Schematic diagram of the experimental setup for UTDR tests.

9. Calculation equations

The penetration depth (d_{wet}) of the MEA solution into the membrane can be calculated as (Luo et al., 2023; Wan et al., 2023),

$$d_{wet} = \frac{V\Delta t}{2} \quad (S5)$$

where V is the velocity of ultrasonic waves in the MEA solution, and Δt is the difference in arrival time obtained from UTDR tests.

The effective membrane thickness (d_{eff}) is defined as the thickness of the non-wetted portion of the membrane and is calculated as

$$d_{eff} = d_{mem} - d_{wet} \quad (S6)$$

where d_{mem} is the total membrane thickness, and d_{wet} is the penetration depth obtained from UTDR tests. For the TFC Janus membrane, d_{mem} refers to the thickness of the PVDF substrate, as the PVA layer is hydrophilic.

The air-filled hydrophobic membrane can be modeled as a capacitor, and the capacitance (C_{mem}) can be estimated (Li et al., 2020),

$$C_{mem} = \frac{\varepsilon_0 \varepsilon_m A_{eff}}{d_{eff}} \quad (S7)$$

Thus, the effective gas-liquid interface area (A_{eff}) in the membrane can be calculated,

$$A_{eff} = \frac{C_{mem} d_{eff}}{\varepsilon_0 \varepsilon_m} \quad (S8)$$

where ε_0 and ε_m are the permittivity of air (or vacuum) and the relative permittivity of the air-membrane matrix, respectively.

10. Long-term performance of the TFC Janus membrane

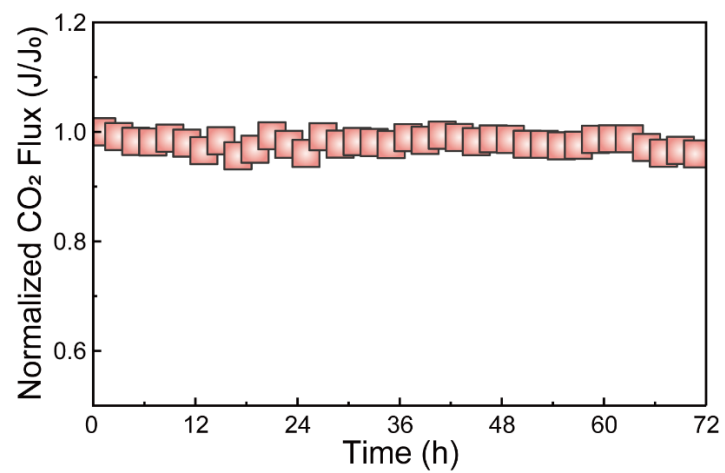


Fig. S9 Normalized CO₂ flux for the TFC Janus membrane in a 72-h GLMC experiment.

1 11. Comparison of the TFC Janus membrane with reported membranes

2 Table S1 Performance comparison of the TFC Janus membrane and representative membranes reported in the literature.

Membranes	Feed gas	Absorbent	CO ₂ flux (mol/m ² /s)	CO ₂ flux reduction	Ref.
PP	CO ₂ /Air (14/86)	20 wt% MEA	0.40×10 ⁻³	66 h, ~ 15%	(Franco et al., 2009)
PP	CO ₂ /Air (15/85)	1 mol/L MEA	0.40×10 ⁻³	-	(Khaisri et al., 2009)
PP	CO ₂ /N ₂ (15/85)	1 mol/L MEA	1.70×10 ⁻³	30 d, ~ 37%	(Wang et al., 2013)
PP	CO ₂ /N ₂ (20/80)	1 mol/L MEA	0.23×10 ⁻³	10 d, ~ 56%	(Lv et al., 2012)
PVDF	CO ₂ /Air (15/85)	1 mol/L MEA	1.46×10 ⁻³	-	(Khaisri et al., 2009)
PVDF	CO ₂ /N ₂ (15/85)	1 mol/L MEA	1.64×10 ⁻³	30 d, ~ 50%	(Wang et al., 2013)
PVDF	CO ₂ /Air (20/80)	2 mol/L MEA	1.26×10 ⁻³	-	(Rongwong et al., 2015)
PVDF	Pure CO ₂	2 mol/L MEA	2.43×10 ⁻³	3 d, ~ 20%	(Atchariyawut et al., 2007)
PVDF	CO ₂ /N ₂ (9/91)	AMP + PZ	1.36×10 ⁻³	2 h, ~ 90%	(Lin et al., 2016)
PVDF	CO ₂ /N ₂ (19/81)	1 mol/L DEA	0.74×10 ⁻³	-	(Gong et al., 2021)
PTFE	CO ₂ /Air (15/85)	1 mol/L MEA	1.82×10 ⁻³	-	(Khaisri et al., 2009)
PTFE	CO ₂ /Air (20/80)	2 mol/L MEA	2.22×10 ⁻³	-	(Rongwong et al., 2015)
PTFE	CO ₂ /N ₂ (20/80)	30 wt% MEA	0.63×10 ⁻³	-	(Bougie et al., 2014)
PTFE	CO ₂ /N ₂ (15/85)	DMEA + PZ	1.55×10 ⁻³	-	(Cao et al., 2019)
PTFE	Pure CO ₂	AHPD + PZ	2.17×10 ⁻³	-	(Bougie et al., 2015)
PTFE	CO ₂ /N ₂ (9/91)	AMP + PZ	2.50×10 ⁻³	16 h, ~ 93%	(Huang et al., 2018)
TFC Janus	CO ₂ /N ₂ (15/85)	1 mol/L MEA	2.85×10 ⁻³	3 d, ~ 4%	This work

3 Note: PP: polypropylene; PVDF: polyvinylidene fluoride; PTFE: polytetrafluoroethylene; MEA: monoethanolamine; DEA: diethanolamine; DMEA:
 4 dimethylethanolamine; PZ: piperazine; AMP: 2-amino-2-methyl-1-propanol; AHPD: 2-amino-2-hydroxymethyl-1,3-propanediol; All CO₂ flux values are unified as
 5 mol/m²/s for comparative purposes.

12. Pore size distributions of the pristine PVDF membrane

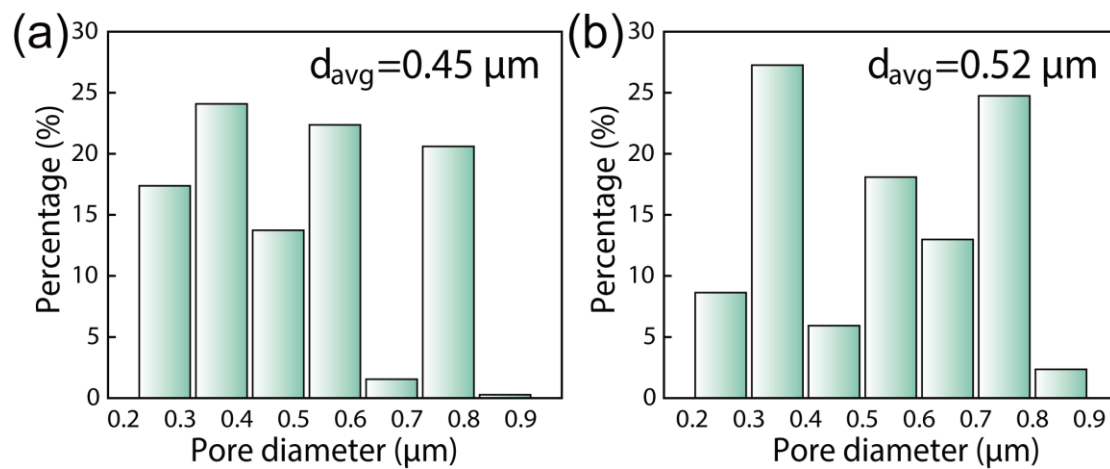


Fig. S10 Pore size distributions of the PVDF membrane (a) before and (b) after a 24-h GLMC experiment.

13. UTDR echo waveforms results

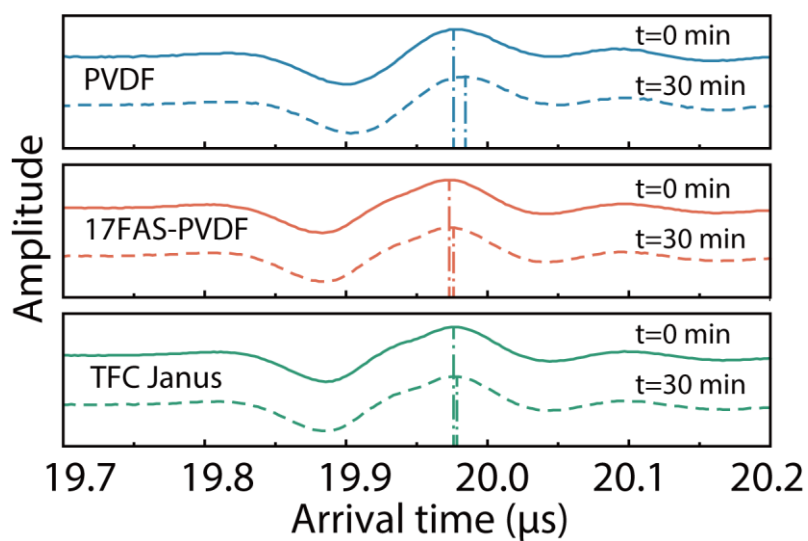


Fig. S11 UTDR echo waveforms of the pristine PVDF membrane, 17FAS-PVDF membrane, and TFC Janus membrane at $t = 0$ min (solid line) and $t = 30$ min (dashed line). In each test, a 1 mol/L MEA solution was used as the testing liquid.

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